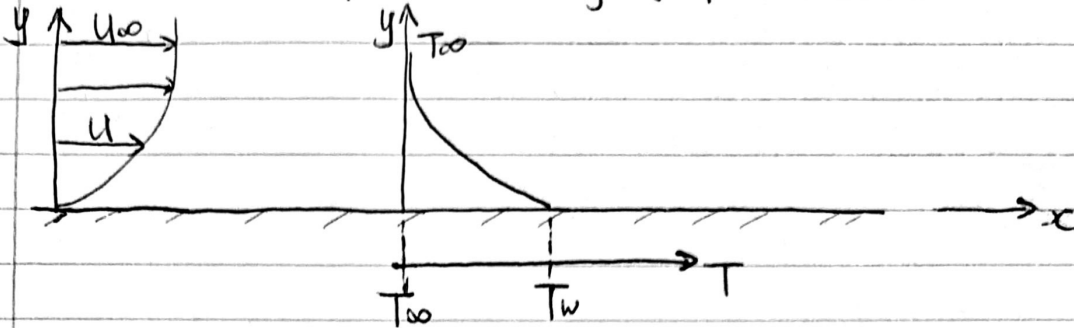


04/02/20

Recap:

When fluid flows over a solid surface, a temperature distribution forms, bridging fluid ( $T_\infty$ ) and the wall ( $T_w$ )



The heat exchange between the wall and the fluid can be expressed as the heat conducted away from the wall by the fluid (Fourier's Law)

$$q = -k_f \left. \frac{\partial T}{\partial y} \right|_{y=0}, \text{ at the wall}$$

$k_f$ : thermal conductivity of the fluid

This defines the convective heat transfer coefficient  $h$

$$-k_f \left. \frac{\partial T}{\partial y} \right|_{y=0} = h \cdot (T_w - T_\infty)$$

It can be seen that in order to obtain  $h$ , we must first obtain  $T(y)$ , which gives us  $\left. \frac{\partial T}{\partial y} \right|_{y=0}$

Aim of Lecture 2: how to solve for  $T$  distribution.

## Lecture 2.

Conservation equations needed to solve for temperature profile:

- <1> Conservation of mass — The continuity equation
- <2> Conservation of momentum — NAVIER-STOKES equation
- <3> Conservation of energy — The energy equation

<1> and <2> We have learnt in Fluid Mechanics.

Brief review :

<1> Continuity equation (for an incompressible fluid)

$$\nabla \cdot \vec{u} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

$u$ ,  $v$ , and  $w$  are the  $x$ ,  $y$ , and  $z$  components of the velocity vector  $\vec{u}$ .

In 2D, the equation reduces to  $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$

<2>  $x$ -direction momentum equation (2D, boundary layer)

$$\underbrace{\frac{\partial u}{\partial t}}_{\text{steady state}} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{dP}{dx} + \frac{\mu}{\rho} \left( \underbrace{\frac{\partial^2 u}{\partial x^2}}_{\text{small}} + \underbrace{\frac{\partial^2 u}{\partial y^2}}_{\substack{\text{neglect,} \\ \text{not in } x\text{-} \\ \text{direction}}} \right) + g$$

reduces to

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{dP}{dx} + \frac{\mu}{\rho} \frac{\partial^2 u}{\partial y^2}$$

we have applied boundary layer approximations

- $\left| \frac{\partial u}{\partial x} \right| \ll \left| \frac{\partial u}{\partial y} \right|$
- $v \ll u$
- $p = f_n(y)$

Bernoulli equation for the mainstream flow above B.L.

$$\frac{p}{\rho} + \frac{u_{\infty}^2}{2} = \text{constant.}$$

↳ The energy equation.

→ extend heat conduction equation to allow for fluid motion

$$\underbrace{\rho c_p \frac{\partial T}{\partial t}}_{\text{energy storage}} = \underbrace{k \nabla^2 T}_{\text{heat conduction}} + \underbrace{\dot{q}}_{\text{heat generation}}$$

$$\text{in 1D: } \rho c_p \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2} + \dot{q}$$

with fluid motion, which carries energy, we need an enthalpy term:

$$\boxed{\underbrace{\rho c_p \frac{\partial T}{\partial t}}_{\text{energy storage}} + \underbrace{\vec{u} \cdot \nabla T}_{\text{enthalpy convection}} = \underbrace{k \nabla^2 T}_{\text{heat conduction}} + \underbrace{\dot{q}}_{\text{heat generation}}}$$

Note:  $\frac{\partial T}{\partial t} + \vec{u} \cdot \nabla T = \frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \frac{DT}{Dt}$

$\frac{D}{Dt}$  is the material derivative.

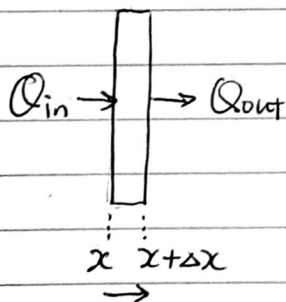
$\frac{DT}{Dt}$  represents change of  $T$  of a fluid particle as it moves.

In a steady, 2D flow, without heat sources,

$$\boxed{u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} + \alpha \frac{\partial^2 T}{\partial x^2}}$$

neglect, since  $\frac{\partial^2 T}{\partial x^2} \ll \frac{\partial^2 T}{\partial y^2}$  in B.L.

Derivation: (1D) control volume



$$\Delta x \dot{q} + Q_{in} - Q_{out} = \text{energy gain}$$

$$Q_{in} = -k \left. \frac{dT}{dx} \right|_x + u \cdot \rho c_p T_{in} \Big|_x$$

$$Q_{out} = -k \left. \frac{dT}{dx} \right|_{x+\Delta x} + u \cdot \rho c_p T_{out} \Big|_{x+\Delta x}$$

$$\text{energy gain} = \rho c_p \frac{dT}{dt} \cdot \Delta x$$

$$\Rightarrow \dot{q} \Delta x - k \left. \frac{\partial T}{\partial x} \right|_x + u \cdot \rho c_p T_{in} \Big|_x + k \left. \frac{\partial T}{\partial x} \right|_{x+\Delta x} - u \rho c_p T_{out} \Big|_{x+\Delta x} = \rho c_p \frac{\partial T}{\partial t} \cdot \Delta x$$

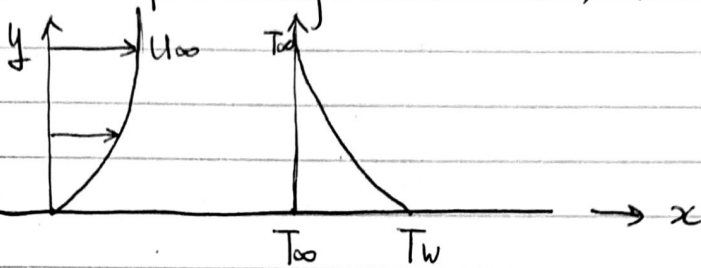
$$\dot{q} + k \left( \frac{\partial T}{\partial x} \Big|_{x+\Delta x} - \frac{\partial T}{\partial x} \Big|_x \right) + u \rho c_p \cdot \left( \frac{T \Big|_x - T \Big|_{x+\Delta x}}{\Delta x} \right) = \rho c_p \frac{\partial T}{\partial t}$$

$$\dot{q} + k \frac{\partial^2 T}{\partial x^2} - u \rho c_p \frac{\partial T}{\partial x} = \rho c_p \frac{\partial T}{\partial t}$$

$$\rho c_p \left( \frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} \right) = k \frac{\partial^2 T}{\partial x^2} + \dot{q}$$

We found that 2D steady energy equation looks very similar to 2D momentum equation (with no pressure variation)!

Consider B.L. in a fluid with bulk  $U_\infty$  and  $T_\infty$  flowing over a flat surface at  $T_w$ , without a pressure gradient.



momentum :

$$u \frac{\partial}{\partial x} \left( \frac{u}{U_\infty} \right) + v \frac{\partial}{\partial y} \left( \frac{u}{U_\infty} \right) = \nu \frac{\partial^2}{\partial y^2} \left( \frac{u}{U_\infty} \right) \quad \dots \textcircled{1}$$

kinetic viscosity

$$\text{B.C.} \begin{cases} y=0, & \frac{u}{U_\infty} = 0 \\ y=\infty, & \frac{u}{U_\infty} = 1 \\ y=\infty, & \frac{\partial}{\partial y} \left( \frac{u}{U_\infty} \right) = 0 \end{cases}$$

$\frac{u}{U_\infty}$ : dimensionless
$\frac{u}{U_\infty}$ : velocity

energy : define dimensionless temperature  $\Theta = \frac{T - T_w}{T_\infty - T_w}$

$$u \frac{\partial \Theta}{\partial x} + v \frac{\partial \Theta}{\partial y} = \alpha \frac{\partial^2 \Theta}{\partial y^2} \quad \dots \textcircled{2}$$

thermal diffusivity

$$\text{B.C.} \begin{cases} y=0, & \Theta = 0 \\ y=\infty, & \Theta = 1 \\ y=\infty, & \frac{\partial \Theta}{\partial y} = 0 \end{cases}$$

equation  $\textcircled{1}$  and  $\textcircled{2}$  are identical with the same B.C.  
only difference is  $\nu$  and  $\alpha$ !

The solution to  $\Theta$  is  $\frac{u}{u_{\infty}} = f'(\eta)$  where  $\eta = \sqrt{\frac{u_{\infty}}{\nu x}} y$   
and  $f(\eta)$  (Blasius problem)

If  $\alpha = \nu$ , then  $\Theta$  is the same with  $\frac{u}{u_{\infty}}$ .

We can immediately calculate  $h$ :

$$h = \frac{k}{T_{\infty} - T_w} \left. \frac{\partial (T - T_w)}{\partial y} \right|_{y=0} = k \left. \frac{\partial \Theta}{\partial y} \right|_{y=0} = k \left( \frac{\partial^2 f}{\partial \eta^2} \right) \left. \frac{\partial \eta}{\partial y} \right|_{\eta=0}$$

$\overset{=0.332}{\left( \frac{\partial^2 f}{\partial \eta^2} \right)} \cdot \left. \frac{\partial \eta}{\partial y} \right|_{\eta=0} = \frac{\sqrt{Re_x}}{x}$

$$h = 0.332 \cdot k \cdot \frac{\sqrt{Re_x}}{x}$$

or,  $\frac{hx}{k} = Nu_x = 0.332 \sqrt{Re_x}$